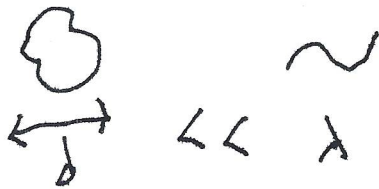


YS 110B 04 Nov 20

Hertzian Multipoles



far-field expansion in terms of multipoles

$$\int \frac{1}{2} \left((\hat{R} \cdot \vec{x}') \vec{J} + (\hat{R} \cdot \vec{J}) \vec{x}' \right) d^3x' = -\frac{i\omega}{2} \int \vec{x}' (\hat{R} \cdot \vec{x}') \rho(\vec{x}') d^3x'$$

$$J \sim e^{-i\omega t}$$

$$\text{Ez contribution } A(\vec{x}) = \frac{-\mu_0 c k^2}{8\pi} \frac{e^{ikr}}{r} \left(1 - \frac{1}{ikr} \right) \int \vec{x}' (\hat{R} \cdot \vec{x}') \rho(\vec{x}'; \omega) d^3x'$$

$$\text{far-field, } \vec{H}(\vec{x}) = \frac{ik \hat{R} \times \vec{A}}{\mu_0}$$

$$\vec{E} = \frac{ik Z_0 (\hat{R} \times \vec{A}) \times \hat{R}}{\mu_0}$$

$$\vec{H} = \frac{-i\omega k^2}{8\pi} \frac{e^{ikr}}{r} \int d^3x' (\hat{R} \times \vec{x}') (\hat{R} \cdot \vec{x}') \rho(\vec{x}'; \omega)$$

α electric quadrupole moment

$$Q_{\alpha\beta} = \int (3x'_\alpha x'_\beta - |\vec{x}'|^2 \delta_{\alpha\beta}) \rho(\vec{x}') d^3x'$$

Q is a symmetric 3x3 matrix

$$\hat{R} \times \int \vec{x}' (\hat{R} \cdot \vec{x}') \rho(\vec{x}'; \omega) d^3x' = \dots = \frac{1}{3} \hat{R} \times (Q \hat{R})$$

$$\vec{H}(\vec{x}) = \frac{-i\omega k^3}{24\pi} \frac{e^{ikr}}{r} \hat{R} \times Q \hat{R}$$

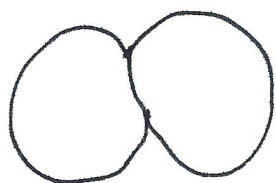
far field

Poynting vector \Rightarrow

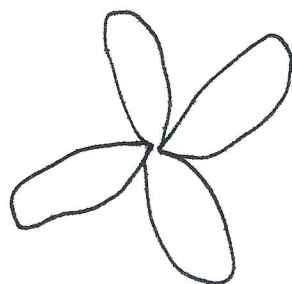
$$\frac{\Delta P}{\Delta \Omega} = \frac{c^2 Z_0 k^6}{1152 \pi^2} |\hat{R} \times \hat{A} \times \hat{R}|^2 ; \hat{R} = \hat{r} \text{ line of sight from the origin to the observation point}$$

$$\Rightarrow P = \frac{c^2 Z_0 k^6}{1440 \pi} \sum_{\alpha, \beta} |A_{\alpha\beta}|^2 \text{ power radiated at } \omega$$

$$A \sim q d^2 \sim \frac{I}{\omega} d^2 \quad P \sim k^4 I^2 d^4$$



dipole shape



quadrupole shape

Each new term pair brings in a pair of poles, one for magnetic and the other electric

Vector spherical Harmonics
(orthogonal basis of vector fields) } an aside
more in grad school

$$\lim_{r \rightarrow \infty} \iint \vec{S} \cdot \hat{r} da = P$$

\vec{S} has non-radial components $\frac{\vec{E} \times \vec{B}^*}{\mu_0}$

Are either \perp to \hat{r} and/or are imaginary

$$\frac{1}{2} \text{Re} \frac{\vec{E} \times \vec{B}^*}{\mu_0} = \text{power}$$

real components - radiation
"resistive" components

imaginary components \rightarrow reactive components
represent reactive sloshing of the fields
but don't reach out away from the source

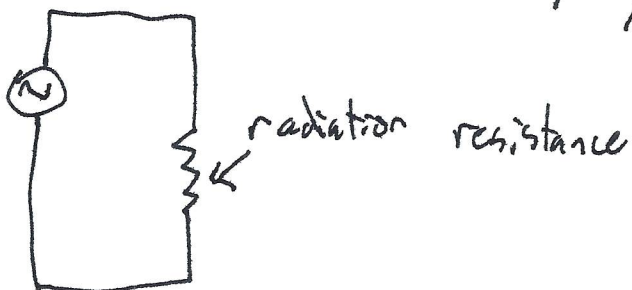
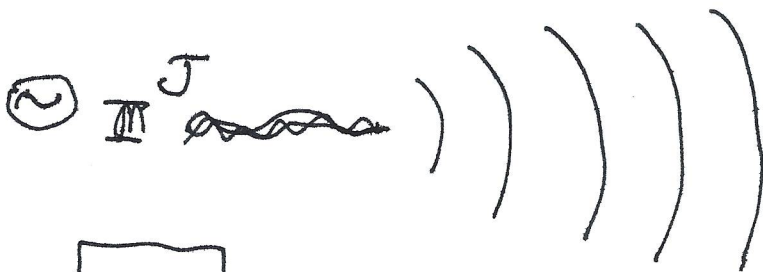
radiated power $P_{rad} \sim Z_0 \cdot \text{const.} \cdot I^2$



impedance of free space (Ohms)

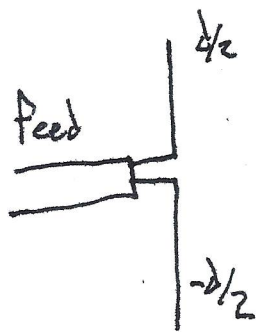
$$P_{resistor} = \text{Re}(Z) I^2$$

radiation resistance of the source



Hertzian $d \ll \lambda \Rightarrow |v| \ll c$

Antennas typically $d \approx \lambda$



if $d \ll \lambda$ antenna looks like a Hertzian dipole

$$d \sim \frac{\lambda}{2} \text{ or } d \approx \lambda$$

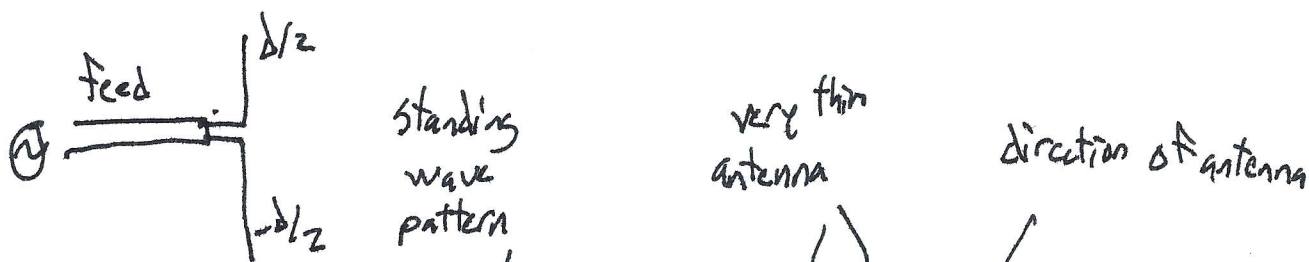
Antenna theory is vast and complicated

dipole antenna

thin, dipole antenna made from a very good conductor with a small gap

Also assuming antenna is thin enough so that the damping due to the radiation is small

⇒ prescribed, sinusoidal function of time



$$\vec{J}(\vec{x}; \omega) = I \sin\left(\frac{kd}{2} - k|z|\right) \delta(x) \delta(y) \hat{z} e^{-i\omega t}$$

in far zone,

$$\vec{A}(\vec{x}; \omega) = \hat{z} \frac{\mu_0}{4\pi} \frac{e^{ikr}}{r} I \int_{-d/2}^{d/2} \sin\left(\frac{kd}{2} - k|z|\right) e^{-ikz \cos\theta} dz$$

$$\vec{A}(\vec{x}; \omega) = \hat{z} \frac{\mu_0}{4\pi} 2I \frac{e^{ikr}}{r} \left(\frac{\cos\left(\frac{kd}{2} \cos\theta\right) - \cos\left(\frac{kd}{2}\right)}{\sin^2\theta} \right)$$

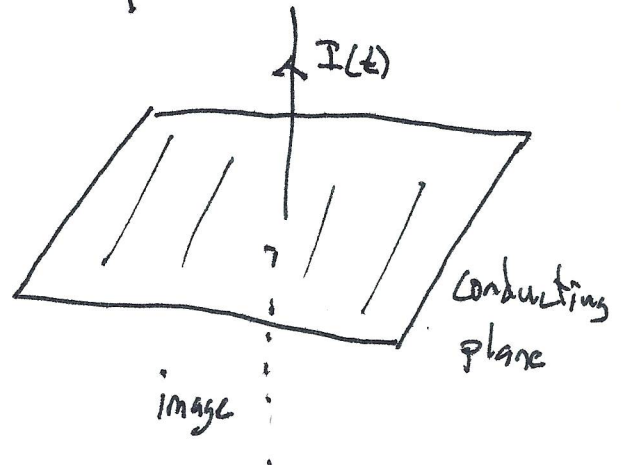
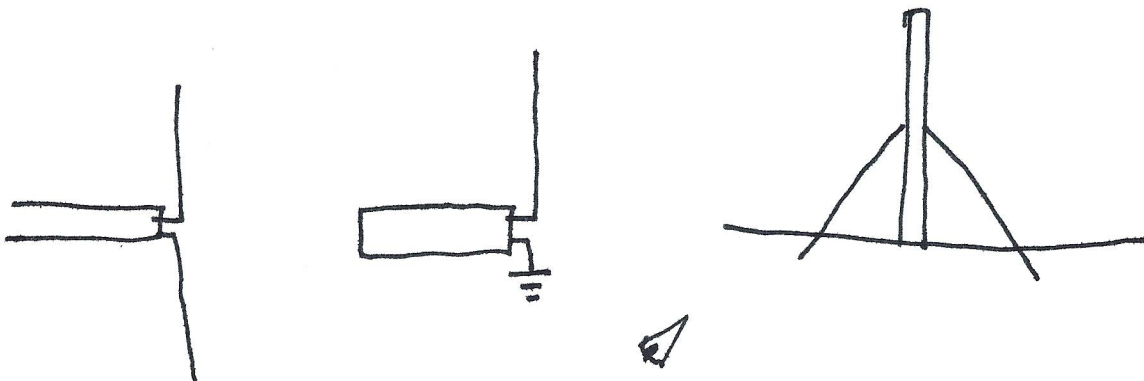
$$\vec{H} = \frac{ik \hat{r} \times \vec{A}}{\mu_0} \quad |\vec{H}| = \frac{k \sin\theta |A_z|}{\mu_0}$$

$$\Rightarrow \frac{dP}{d\Omega} = \dots = \frac{Z_0}{8\pi^2} I^2 \left(\frac{\cos\left(\frac{kd}{2} \cos\theta\right) - \cos\left(\frac{kd}{2}\right)}{\sin\theta} \right)^2$$

$kd \ll 1$ reduces to Hertzian dipole case

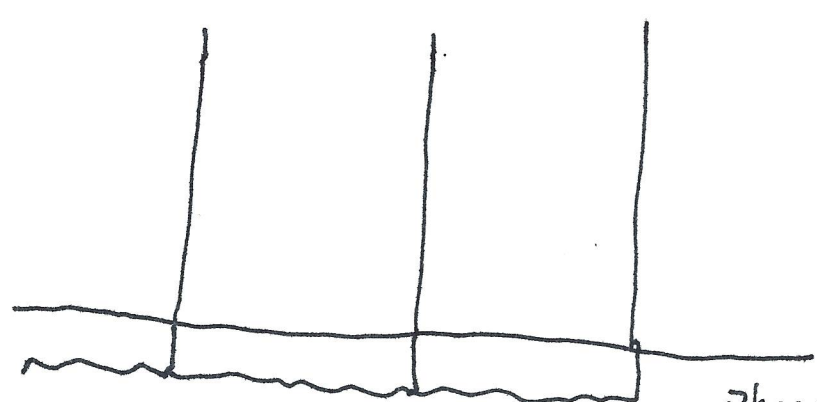
$$\frac{dP}{d\Omega} = \frac{Z_0 I^2}{8\pi} \begin{cases} \frac{\cos^2\left(\frac{\pi}{2} \cos\theta\right)}{\sin^2\theta} & \text{if } kd = \pi \\ \frac{4 \cos^4\left(\frac{\pi}{2} \cos\theta\right)}{\sin^2\theta} & \text{if } kd = 2\pi \end{cases}$$

not only answers but the most popular



ground is pretty good conductor
can see the ~~mirror~~ image of the current too,

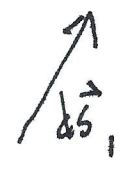
why need 3 or more antennas?



Phase delay the signal
constructive + destructive interference

Can Make them more directional

Reciprocity good emitters make for good receivers



emf induced in ds_1 by current in ds_2

$$\Delta \mathcal{E} = \dots = \frac{i\mu_0}{4\pi} \frac{[I]}{r} [(\hat{r} \times ds_1) \cdot (\hat{r} \times ds_2)]$$

symmetric under interchanging the roles of wire 1 and 2